

- microstrip transmission lines—II: Evaluation of coupled line parameters," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-18, pp. 222–228, April 1970.
- [6] G. Kowalski and R. Pregla, "Calculation of the distributed capacitances of coupled microstrips using a variational integral," *AEU*, vol. 27, pp. 51–52, 1973.
- [7] H. G. Bergand and R. Pregla, "Calculation of the even- and odd-mode capacitance parameters for coupled microstrips," *AEU*, vol. 26, pp. 153–158, 1972.
- [8] R. Pregla, "Calculation of the distributed capacitances and phase velocities in coupled microstrip lines by conformal mapping techniques," *AEU*, vol. 26, pp. 470–474, 1972.
- [9] K. N. Shamanna *et al.*, "Parallel-coupled microstrip line is easy to determine with nomograms," *Electron. Design*, vol. 11, pp. 78–81, May 24, 1976.
- [10] S. D. Shamasundara and N. Singh, "Design of coupled microstrip lines," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-25, pp. 232–233, Mar. 1977.
- [11] S. Akhtarzad *et al.*, "The design of coupled microstrip lines," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-23, pp. 486–492, June 1975.
- [12] A. E. Ros, "Design charts for inhomogeneous coupled microstrip lines," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-26, pp. 394–400, June 1978.
- [13] T. G. Bryant and J. A. Weiss, "Parameters of microstrip transmission lines and coupled pairs of microstrip lines," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-16, pp. 1021–1027, Dec. 1968.
- [14] H. Howe, Jr., *Stripline circuit design*. MA: Artech-House, 1974.
- [15] A. Schwarzmann, "Microstrip plus equations add up to fast designs," *Electron.*, vol. 40, pp. 109–112, Oct. 2, 1967.
- [16] J. A. Weiss and T. G. Bryant, *Microwave Engineer's Handbook*. vol. 1, T. S. Saad, Ed., MA: Artech-House, 1971.
- [17] R. P. Coats, "An octave-band switched-line microstrip 3-b diode phase shifter," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-21, pp. 444–449, July 1973.
- [18] H. A. Wheeler, "Transmission-line properties of a strip on a dielectric sheet on a plane," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-25, pp. 631–647, Aug. 1977.
- [19] R. H. Jansen, "High-speed computation of single and coupled microstrip parameters including dispersion, high-order modes, loss and finite strip thickness," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-26, pp. 75–82, Feb. 1978.
- [20] M. K. Krage and G. I. Haddad, "Frequency dependent characteristics of microstrip transmission lines," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-20, pp. 678–688, 1972.
- [21] G. Kowalski and R. Pregla, "Dispersion characteristics of single and coupled microstrips," *AEU*, vol. 26, pp. 276–280, 1972.
- [22] J. B. Knorr and A. Tufekcioglu, "Spectral domain calculations of microstrip characteristics," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-23, pp. 725–728, 1975.
- [23] W. J. Getsinger, "Dispersion of parallel-coupled microstrip," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-21, pp. 144–145, 1973.
- [24] H. J. Carlin and P. P. Civalleri, "A coupled-line model for dispersion in parallel-coupled microstrips," *IEEE Trans. Microwave Theory Tech.*, vol. 23, pp. 444–446, 1975.
- [25] H. A. Wheeler, "Formulas for the skin effect," *Proc. IRE*, vol. 30, pp. 412–424, 1942.
- [26] B. R. Rao, "Effect of loss and frequency dispersion on the performance of microstrip directional couplers and coupled line filters," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-22, pp. 747–750, July 1974.
- [27] E. O. Hammerstad and F. Bekkadal, *Microstrip Handbook*, ELAB Rep. STF44 A74169, Univ. Trondheim, Norway, Feb. 1975.
- [28] M. C. Horton, "Loss calculations for rectangular coupled bars," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-18, pp. 736–738, Oct. 1970.
- [29] R. Garg, "The effect of tolerances on microstripline and slotline performances," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-26, pp. 16–19, Jan. 1978.
- [30] S. D. Shamasundara and K. C. Gupta, "Sensitivity analysis of coupled microstrip directional couplers," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-26, pp. 788–794, Oct. 1978.

## Letters

### Slot Coupling Between Uniform Rectangular Waveguides

A. J. SANGSTER

**Abstract**—The results of a recent paper, which analyzes the slot-coupled waveguide problem using a 'reaction' method, are shown to be at variance with those of more established theories, for the particular case of a centrally located transverse slot in the common broad wall separating a pair of rectangular waveguides.

The boundary value problem comprising a pair of contiguous uniform rectangular waveguides connected electromagnetically by an aperture in the common wall, is a classical problem which has received considerable attention in the literature [1]–[7]. In general, the increasingly elaborate methods of solution which are presented have enabled more complex geometries to be examined, and more accurate results to be achieved. The more

recent techniques, which rely on variation [5], [6] and moment [7] methods, have evolved, and become popular, as a direct consequence of the increasing availability of high-speed digital computers.

Calculations have been performed, using several of the above methods, of the coupling coefficient  $c_{10}$  (see Fig. 1), associated with a centrally located transverse slot in the common broad wall between a pair of identical rectangular waveguides. The results of these calculations are presented in Fig. 2.

For nonresonant slots ( $l < 0.4\lambda$ ), Bethe's small aperture theory [1], modified by the resonance correction suggested by Levy [8], is a well-established and reliable analytical tool. The variational method of Sangster [5], and the moment method of Vu Khac [7], are in good agreement with the Bethe predictions over this range of slot sizes. The measured polarizabilities of Cohn [9] have been employed in the Bethe calculations to achieve this measure of agreement.

The curve of  $c_{10}$  versus slot length generated using the quasi-static antenna method, due to Lewin [3], is in general agreement with the variational and moment-method results, except

Manuscript received February 1, 1979.

The author is with the Department of Electrical and Electronic Engineering, Heriot-Watt University, 31-35 Grassmarket, Edinburgh, Scotland.

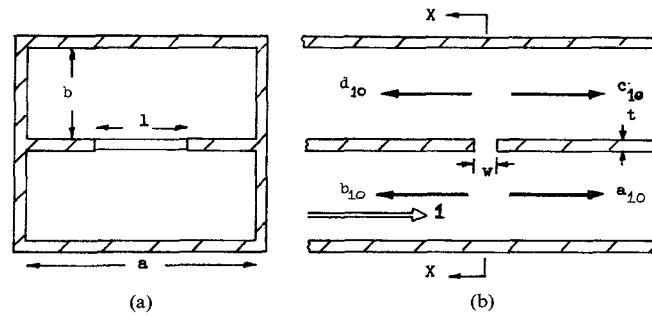


Fig. 1. Waveguide coupler schematic. (a) End section on XX. (b) Side section.

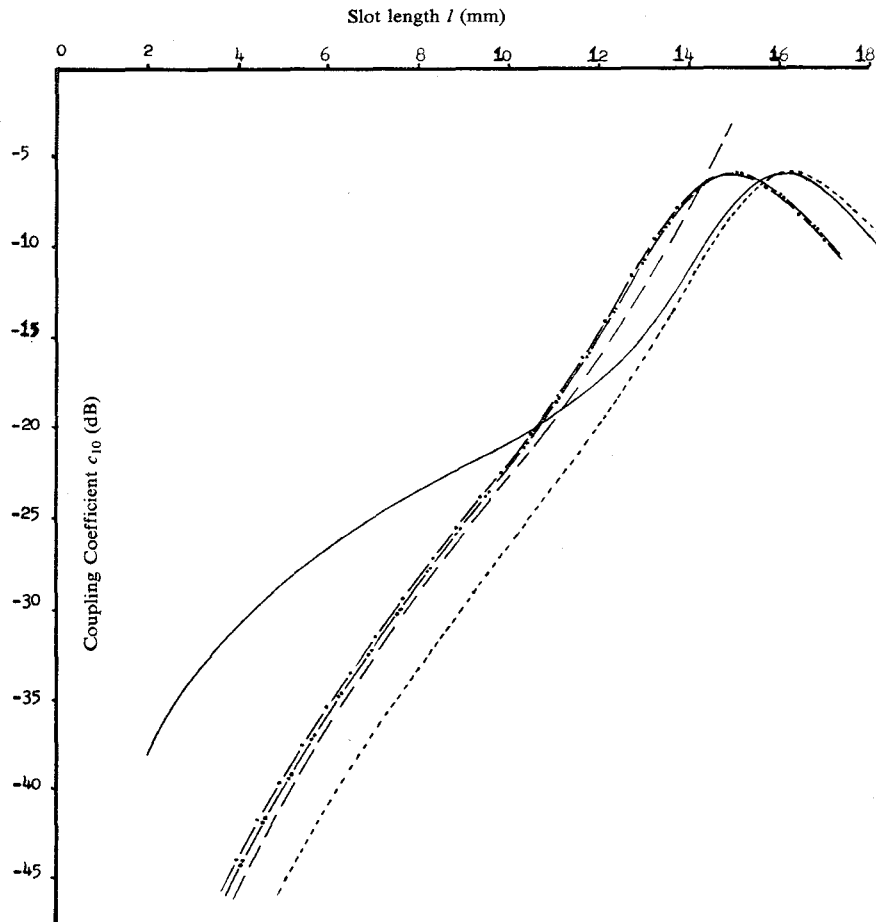


Fig. 2. Coupling versus slot length for a centrally located transverse slot in the common broad wall between a pair of rectangular waveguides, with  $a = 22.86$  mm,  $b = 10.16$  mm,  $w = 1.5875$  mm,  $t = 0.0$  mm,  $\lambda = 32.0$  mm.

- Bethe theory with resonance correction
- - - Variational method [5]
- · - Moment method [7]
- · · Lewin [3]
- Reaction method [10]

for an overall shift of the curve towards longer slot lengths by a distance of approximately  $\lambda/30$ . This discrepancy can be attributed to shortcomings in the strip antenna model, which are discussed by Lewin. This technique predicts that resonance will occur at  $l = \lambda/2$ , and that at resonance  $c_{10} = 0.5$ . The variational and moment methods agree with this latter figure but predict that resonance will occur at  $l = 0.47\lambda$ , a result which is supported

by Oliner [4], when resonance is interpreted as the condition for zero susceptance at the slot.

Superimposed on Fig. 2 is a curve of  $c_{10}$  versus slot length  $l$ , which has been produced using the "reaction" method of Pandharipande and Das [10]. While showing the correct general behavior near resonance, these new results are considerably at variance with those produced by the more established methods

for slots which are small compared to the free-space wavelength. The reaction method was originally propounded by Das and Sanyal [11] as a means of analyzing long slots ( $l > \lambda/2$ ). The suggested trial function for the  $E$ -field in the slot, while obviously appropriate for slots in this category, appears to be seriously in error for short slots. This is supported by Vu Khac's computations, which show [7] that for short nonresonant slots the aperture field is almost perfectly cosinusoidal. In addition, the effect of the side wall on the energy stored inside the waveguide is ignored in this "reaction" method, and it is suggested that for small slots which are almost purely reactive this could be a significant omission.

It is perhaps pertinent to point out here that the specific suggestion, made in [10], that the variational method of [5] is significantly in error near resonance, is patently incorrect. The apparent discrepancy detected by Pandharipande can be traced to an unfortunate printing error in the published paper. This error can be isolated without difficulty by performing a dimensional check on eq. (34), or by consulting fig. 4 of [5] which was extracted directly from the original thesis describing the variational method [12]. Equation (34) of [5] should read

$$c_{10} = -d_{10} = \frac{AP(I_1 + h_1 J_1)^2}{(X + jY)(I_1 + h_1 J_1)^2 - j \sum_{m=1}^{\infty} \sum_{n=0}^{\infty} Q_{mn}(I_m + h_1 J_m)^2} \quad (1)$$

where  $A = 1$  is the amplitude of the incident wave,

$$P = \frac{F^2 ab \sin^2 \beta w \sin^2 \frac{\pi s}{a}}{\omega \epsilon_0}$$

$$X = \frac{2}{\beta^3} \left( 1 - \frac{\pi^2}{a^2 k_0^2} \right) \sin^2 \frac{\pi s}{a} (\cos 2\beta w - 1)$$

$$Y = \frac{2}{\beta^3} \left( 1 - \frac{\pi^2}{a^2 k_0^2} \right) \sin^2 \frac{\pi s}{a} (2\beta w - \sin 2\beta w)$$

$$Q_{mn} = \frac{c_0}{\alpha_{mn}^3} \left( 1 - \frac{m^2 \pi^2}{a^2 k_0^2} \right) \sin^2 \frac{m\pi s}{a} \cdot [4\alpha_{mn} w - 2(1 - \exp(-2\alpha_{mn} w))]$$

$$c_0 = \begin{cases} = 0, & \text{for } n=0; m=1 \\ = 1, & \text{for } n=0; m>1 \\ = 2, & \text{for } n>0; m>1 \end{cases}$$

$$I_m = \int_{-\pi/2}^{\pi/2} \cos m\alpha\theta \cos \theta d\theta$$

$$= \begin{cases} \pi/2, & \text{when } m\alpha = \frac{2ml}{a} = 1 \\ \frac{2}{1 - m^2 \alpha^2} \cos \frac{m\pi\alpha}{2}, & \text{when } m\alpha \neq 1 \end{cases}$$

$$J_m = \int_{-\pi/2}^{\pi/2} \cos m\alpha\theta \cos 3\theta d\theta$$

$$= \begin{cases} \pi/2, & \text{when } m\alpha = 3 \\ \frac{6}{m^2 \alpha^2 - 9} \cos \frac{m\pi\alpha}{2}, & \text{when } m\alpha \neq 3. \end{cases}$$

At resonance the coupling coefficient  $c_{10}$  will be real, which implies that the imaginary terms in the denominator of (1) must sum to zero. Thus at resonance the variational method gives

$$c_{10} = \frac{P}{X} = \frac{\beta^2}{2\omega \epsilon_0 k_0 Z_0 \left( 1 - \frac{\pi^2}{a^2 k_0^2} \right)} \quad (2)$$

But

$$\beta^2 = k_0^2 - \frac{\pi^2}{a^2} \quad \text{and} \quad k_0 Z_0 = \omega \mu_0$$

thus at resonance,  $c_{10} = 0.5 = -6$  dB, and this is in exact agreement with Pandharipande's resonance value for  $c_{10}$ .

## REFERENCES

- [1] H. A. Bethe, "Theory of diffraction by small holes," *Phys. Rev.*, vol. 66, pp. 163-182, 1944.
- [2] A. F. Stevenson, "Theory of slots in rectangular waveguide," *J. App. Phys.*, vol. 19, pp. 24-38, Jan. 1948.
- [3] L. Lewin, "Some observations on waveguide coupling through medium sized slots," *Proc. Inst. Elec. Eng.*, vol. 107C, pp. 171-178, Feb. 1960.
- [4] A. A. Ohner, "The impedance properties of narrow radiating slots in the broad face of rectangular waveguide," *IEEE Trans. Antennas Propagat.*, vol. AP-5, pp. 4-20, Jan. 1957.
- [5] A. J. Sangster, "Variational method for the analysis of waveguide coupling," *Proc. Inst. Elec. Eng.*, vol. 112, pp. 2171-2179, Dec. 1965.
- [6] I. B. Levinson and P. S. Fredberg, "Slot couplers of rectangular one mode waveguide equivalent circuits and lumped parameters," *Radio Eng. Electron. Phys.*, no. 1, pp. 717-724, 1966.
- [7] T. Vu Khac, "Solutions for some waveguide discontinuities by the method of moments," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-20, pp. 416-418, June 1972.
- [8] R. Levy, "Analysis and synthesis of waveguide multi-aperture directional couplers," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-16, pp. 995-1006, Dec. 1968.
- [9] S. B. Cohn, "Determination of aperture parameters by electrolytic tank measurements," *Proc. IRE*, vol. 39, pp. 1416-1421, Nov. 1951.
- [10] V. M. Pandharipande and B. N. Das, "Coupling of waveguides through large apertures," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-26, pp. 209-212, Mar. 1978.
- [11] B. N. Das and G. S. Sanyal, "Network parameters of a waveguide broadwall slot radiator," *Proc. Inst. Elec. Eng.*, vol. 117, pp. 41-44, 1970.
- [12] A. J. Sangster, "A variational analysis of waveguide coupling," M.Sc. Thesis, University of Aberdeen, Aberdeen, Scotland, Oct. 1964.

## Comments on "Coupling of Waveguides Through Large Aperture"

V. M. PANDHARIPANDE AND B. N. DAS

The authors thank Dr. Sangster for his useful comments<sup>1</sup> on their paper [1]. At the time of preparation of the paper it was not known to the authors that there was an unfortunate printing

Manuscript received April 20, 1979.

The authors are with the Department of Electronics and Electrical Communication Engineering, Indian Institute of Technology, Kharagpur 721302, India.

<sup>1</sup>A. J. Sangster, "Slot coupling between uniform rectangular waveguides," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-27, pp. 705-707, July 1979.